

# Electronics Case Studies

## Applications:

- Thermal Management
- Semiconductor Manufacturing
- Lighting
- Avionics
- Telecommunications
- Computers
- Consumer Products

## Results:

- Improved Performance
- Reduced Risk and Cost
- Greater Safety and Life
- Faster Design Turnaround
- More Robust Designs
- Increased Innovation



# Customer Success: Lighting Heat Management

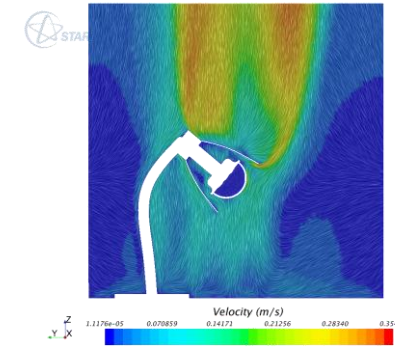
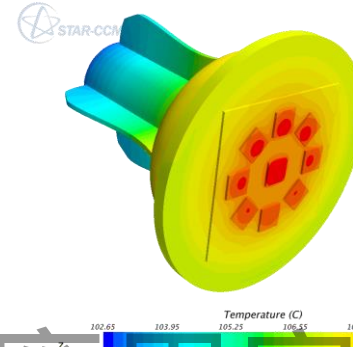
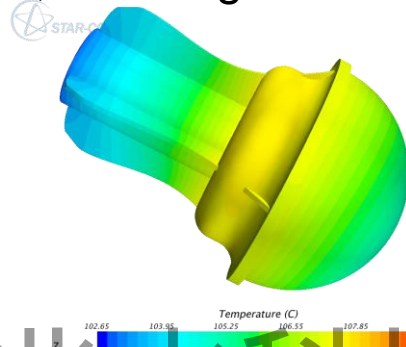
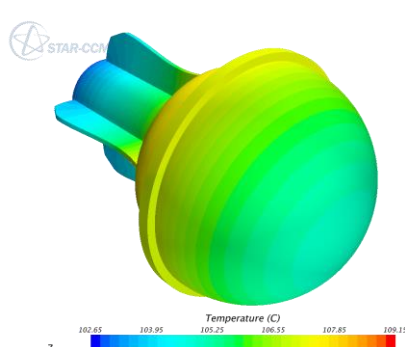
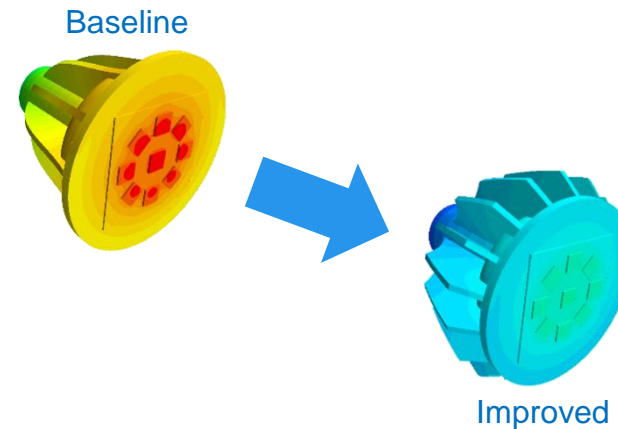


## Challenge:

- Improve heat sink for indoor aluminum LED bulb (9 LEDs emitting 4.8W each)
  - Minimize heat sink mass
- Constraints
  - Temperature of bulb  $\leq 100$  C, ambient = 22C
- Design variables
  - Thickness, shape, fins of heat sink

## Results:

- Identified lowest mass design per specifications
- Result obtained after 72 hours, 50 designs



# Customer Success: LED Cooling Design Study

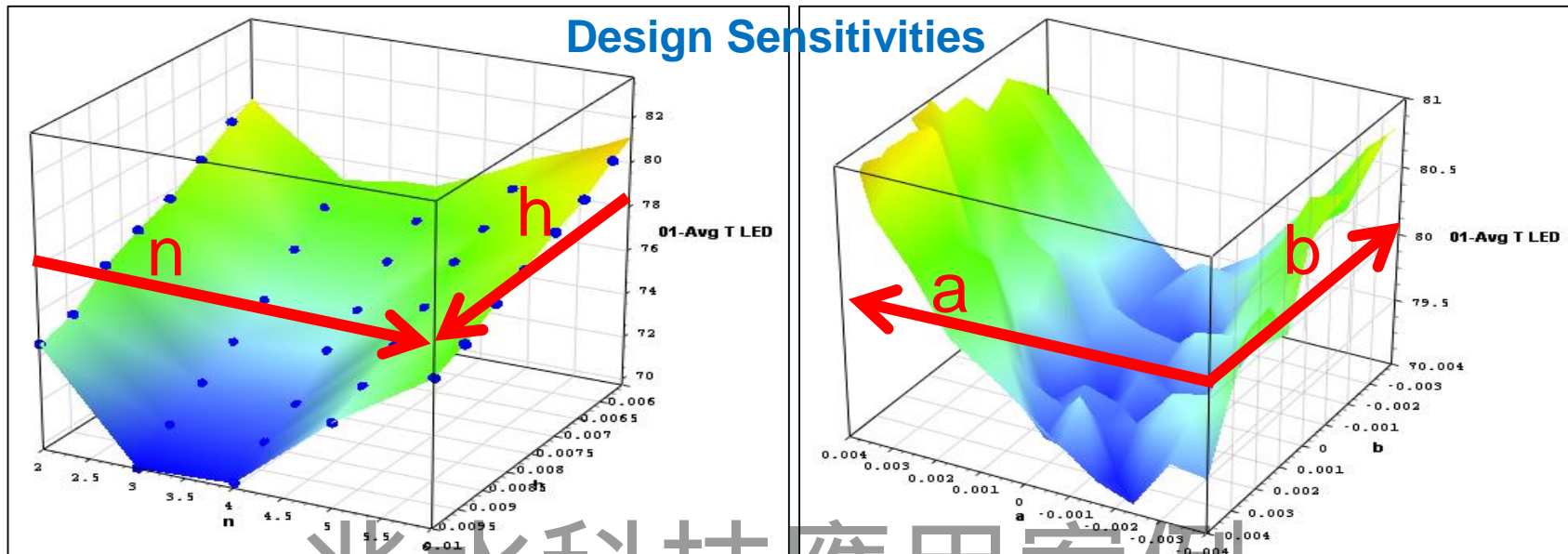
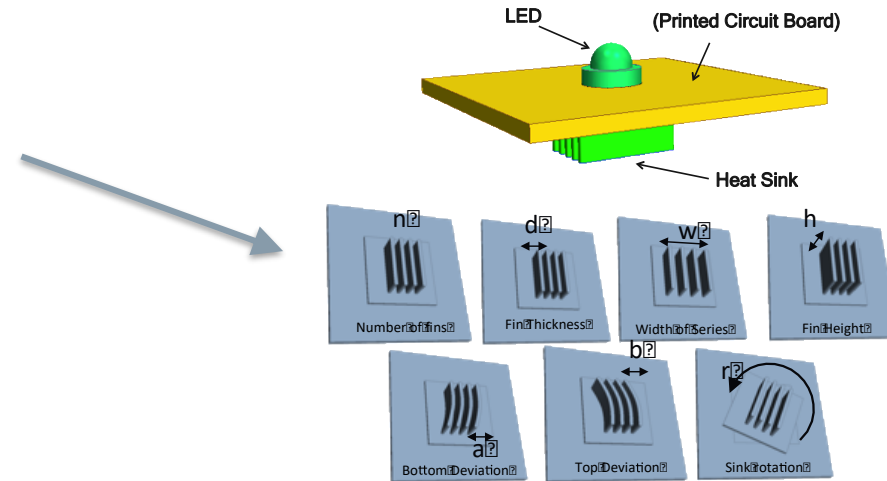


## Challenge:

- Design a heat sink to minimize LED temperature
- Design variables (7): sink geometry

## Results:

- 700 evaluations
- LED Temp reduced >21%



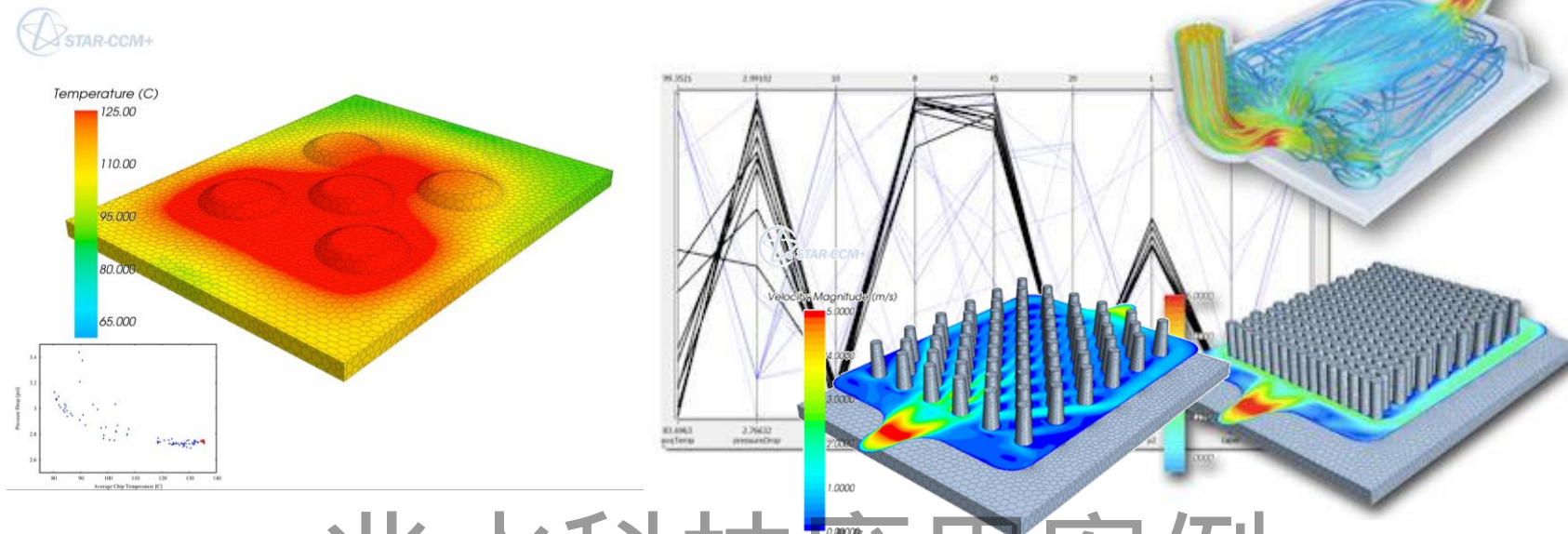
# Customer Success: Electronics Cooling Design

## Challenge:

- Minimize chip temperature and pressure drop in ethylene glycol cooling fluid
- Design variables
  - Number, size, spacing, and taper of heat exchanger pins

## Results:

- Reduced chip temperature by 13 °C



# 兆水科技應用案例

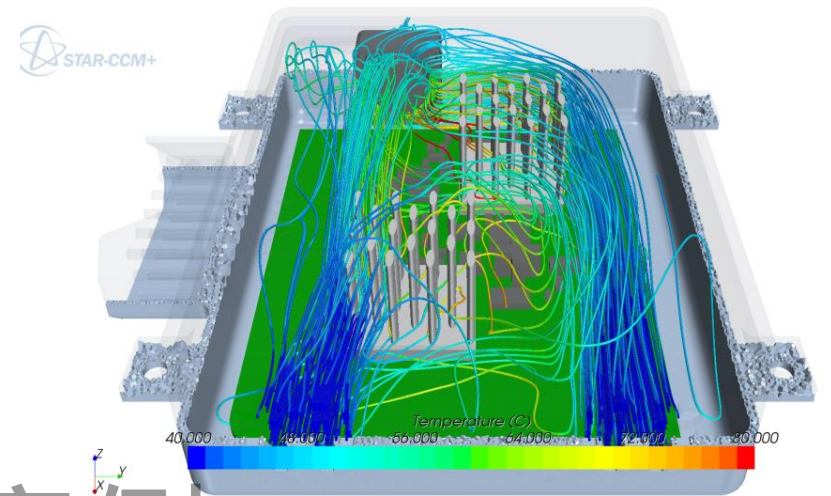
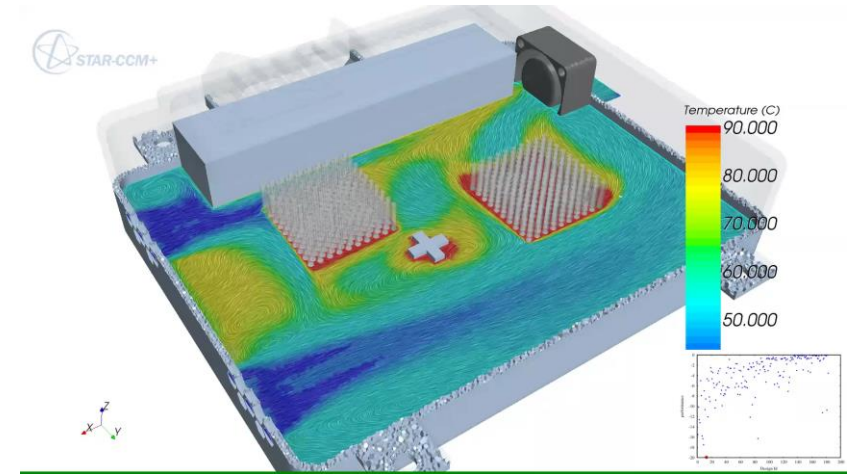
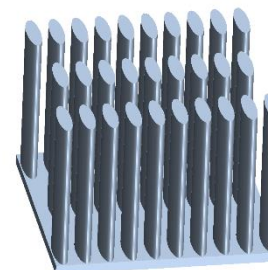
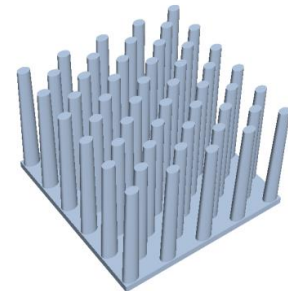
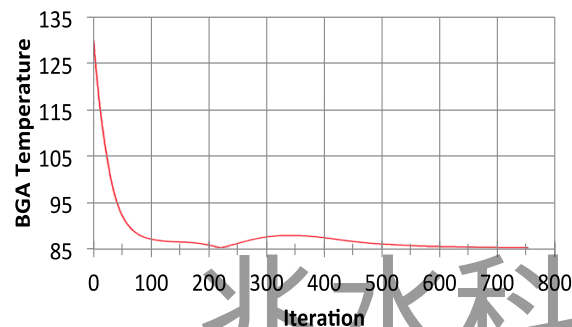
# Customer Success: Computer Cooling Design Study

## Challenge:

- Improve geometry of IC heat sink
  - Minimize heat sink mass (weighted 25%)
  - Minimize difference between temp and 85 deg. (75%)
- Constraints
  - Ambient temp = 40 deg.
  - Fixed fan speed
  - Maximum values for pin geometry
- Design variables
  - Pin height, radii, taper, density

## Results:

- Identified best cooling pin layout and fan location



# Customer Success: Avionics Air Transport Rack Study

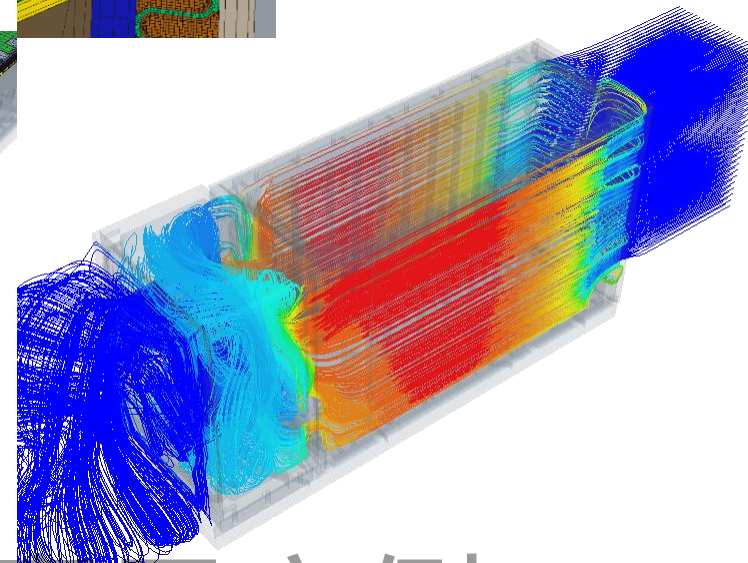
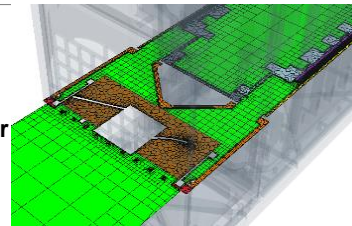
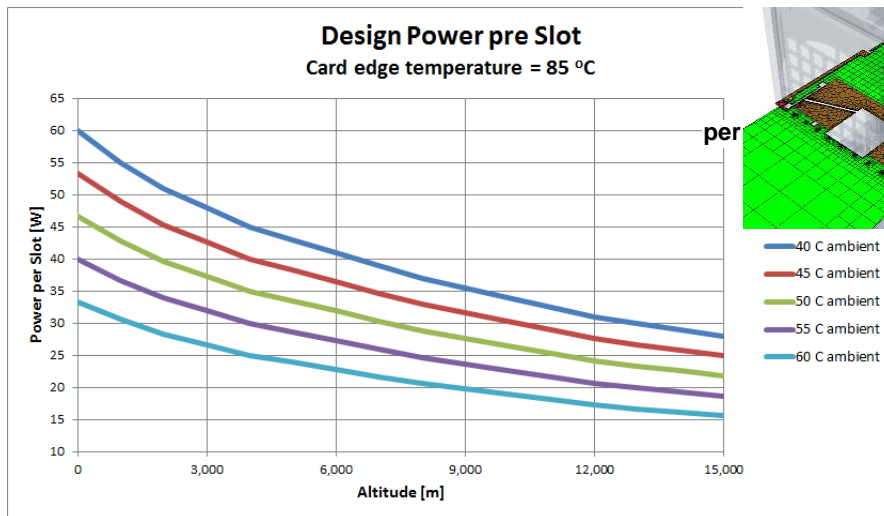
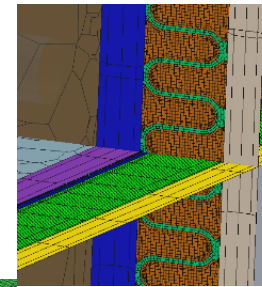
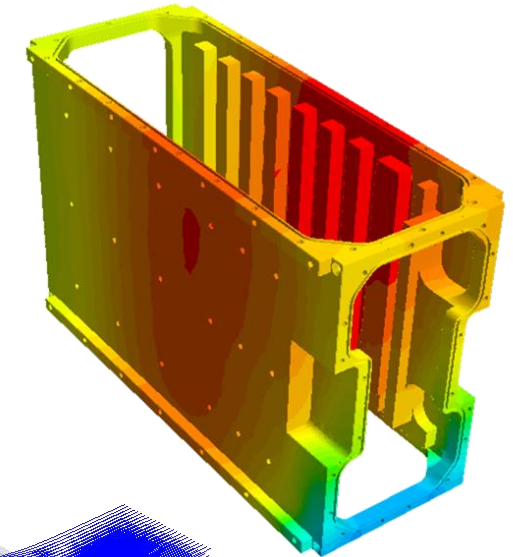


## Challenge:

- Identify the maximum power per slot that can be used on an avionics Air Transport Rack (ATR) at different altitudes and temperatures

## Results:

- Eliminated need for expensive testing
- Max power identified at every temp and altitude



# Customer Success: Performance, Range & Comfort



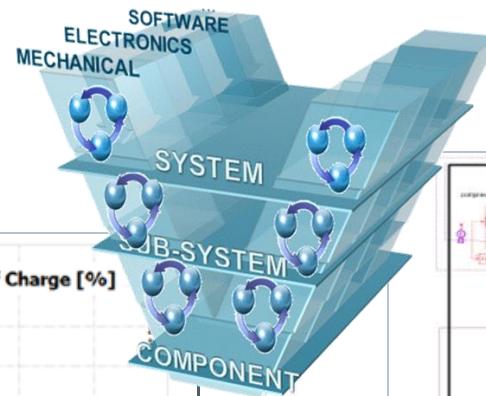
## Challenge:

- Balance performance, range, and passenger comfort of an electric vehicle
- AMESim and Matlab/Simulink used to simulate 1D system behavior
- HEEDS adjust bypass orifice to improve system performance

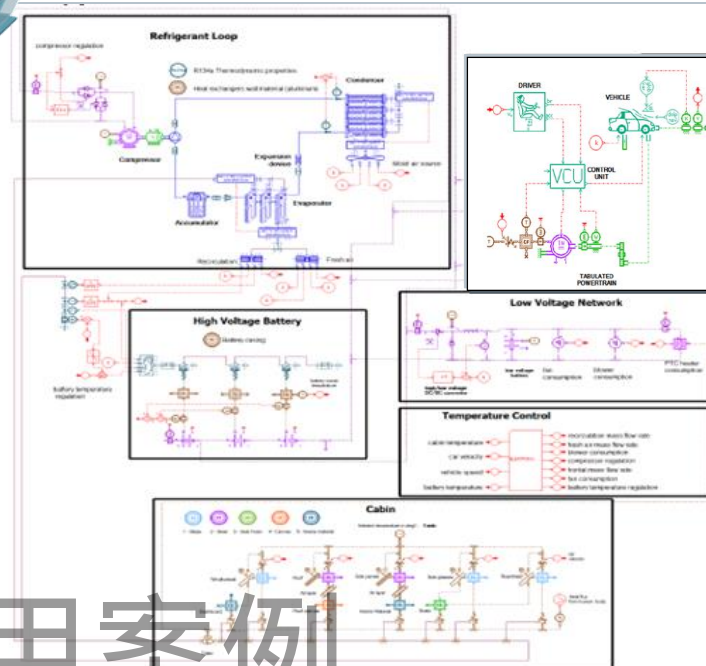
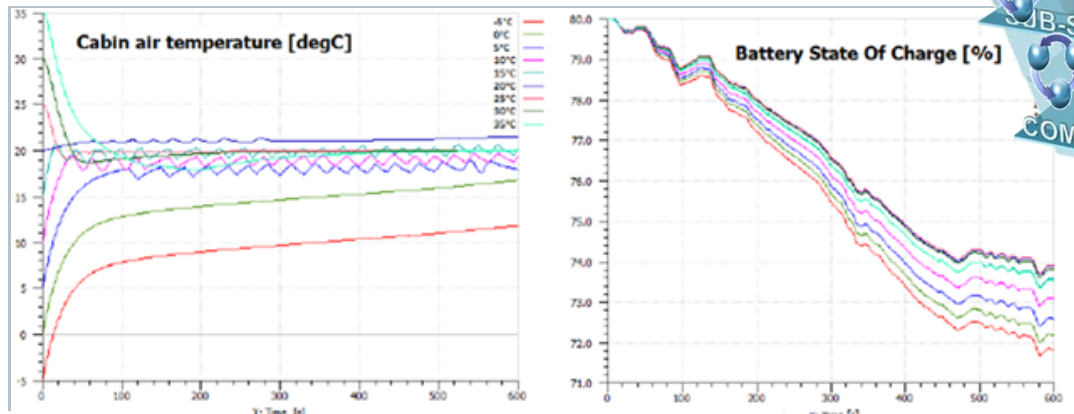


## Results:

- Best balance achieved



AMESim 1-D Subsystem Models



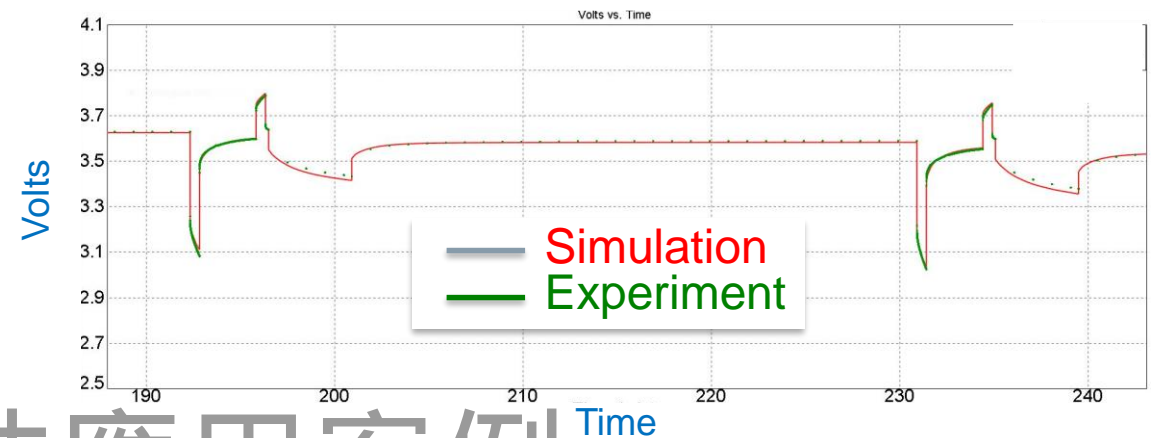
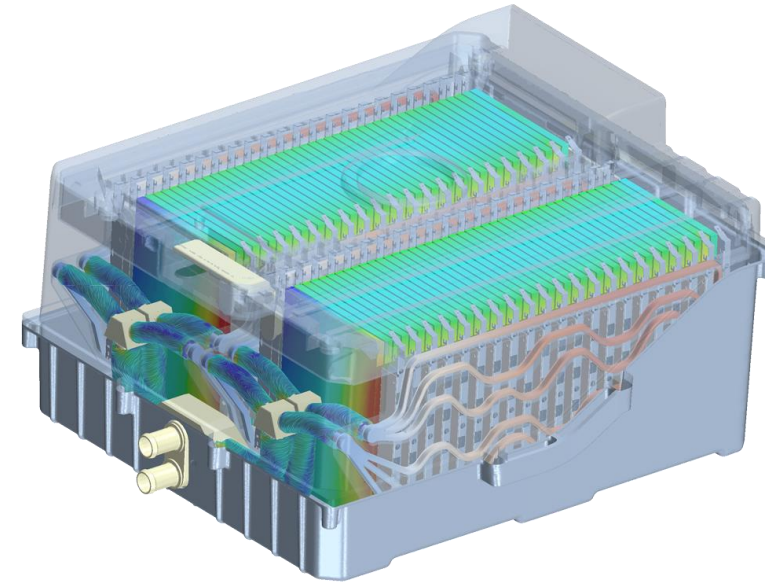
# Customer Success: Battery Performance Correlation

## Challenge:

- Improve battery performance model
  - Minimize RMS error between simulation and test
  - Use Battery Design Studio simulation model
- Design variables (8)
  - NCA diffusion pre-exponential factor
  - Graphite diffusion pre-exponential factor
  - Surface area
  - Separator – MacMullin Number
  - Base Model Tortuosity Negative
  - Base Model Tortuosity Positive
  - SEI Pre-exponential factor

## Results:

- Excellent correlation between simulation and experimental test results



# Customer Success: Electric Motor Design Study



## Challenge

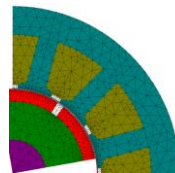
- Minimize cogging torque
- Design variables
  - $100^\circ < \text{Magnet Pole Arc} < 180^\circ$
  - $1 \text{ mm} < \text{Slot Opening (SO)} < 4 \text{ mm}$
  - $0.3 \text{ mm} < \text{Air Gap (Gap)} < 2 \text{ mm}$

## Results

- 99% lower cogging torque

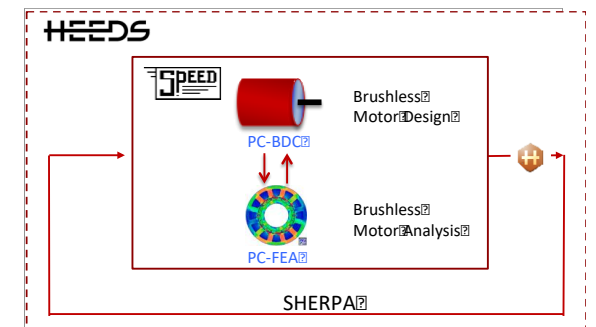
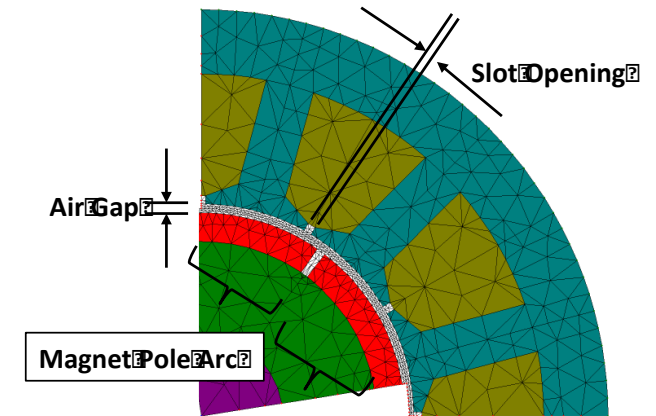
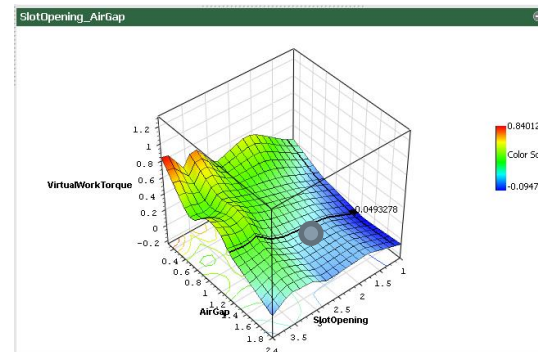
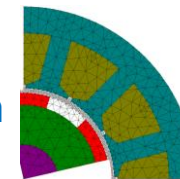
### Baseline Design:

- Cogging Torque= 0.7185 Nm
- Magnet Pole Arc =  $170^\circ$
- Slot Opening (SO) = 3.0 mm
- Air Gap (Gap) = 0.5 mm



### Improved Design:

- Cogging Torque= 0.004 Nm
- Magnet Pole Arc =  $123^\circ$
- Slot Opening (SO) = 1.15 mm
- Air Gap (Gap) = 1.35 mm



# Customer Success: Electric Motor Design Study

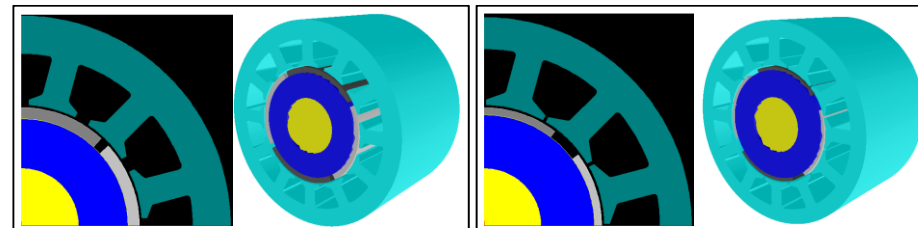
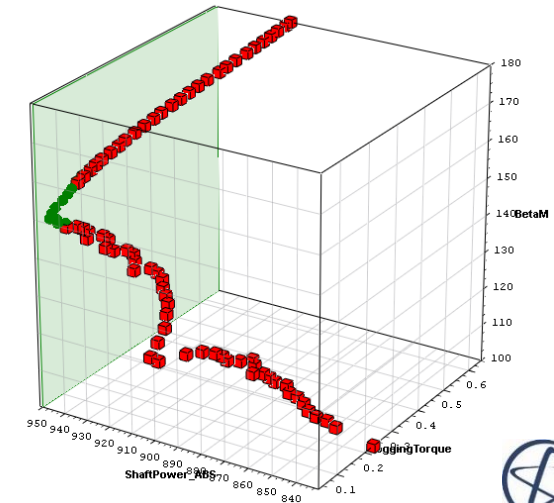


## Challenge:

- Minimize cogging torque and magnet volume
- Constraints (8):
  - $950\text{ W} < \text{Shaft Power} < 1050\text{ W}$
  - $190\text{ V} < \text{Induced Voltage} < 200\text{ V}$
  - Copper Losses  $< 100\text{ W}$
  - Iron Losses  $< 20\text{ W}$
  - Total Losses  $< 120\text{ W}$
  - $1.4\text{ T} < \text{Stator Flux Density} < 1.6\text{ T}$
  - $1.4\text{ T} < \text{Stator Yoke Flux} < 1.6\text{ T}$
  - Rotor Yoke Flux Density  $< 1.6\text{ T}$
- Design variables (10):
  - $100^\circ \leq \text{Magnet Pole Arc} \leq 180^\circ$
  - $1\text{ mm} \leq \text{Slot Opening} \leq 4\text{ mm}$
  - $0.3\text{ mm} \leq \text{Air Gap} \leq 2\text{ mm}$
  - $10\text{ mm} \leq \text{Slot Depth} \leq 17\text{ mm}$
  - $50 \leq \text{Number of Coils} \leq 150$
  - $60\text{ mm} \leq \text{Stack Length} \leq 80\text{ mm}$
  - $4\text{ A} \leq \text{Current Set Point} \leq 7\text{ A}$
  - $5\text{ mm} \leq \text{Tooth Width} \leq 10\text{ mm}$
  - $1\text{ mm} \leq \text{Magnet Thickness} \leq 5\text{ mm}$
  - $26\text{ mm} \leq \text{Outer Rotor Radius} \leq 36\text{ mm}$

## Results:

- 94% reduction in cogging torque
- 46% reduction in magnet volume



Baseline

Optimized (46% Reduction in Magnet Volume)

